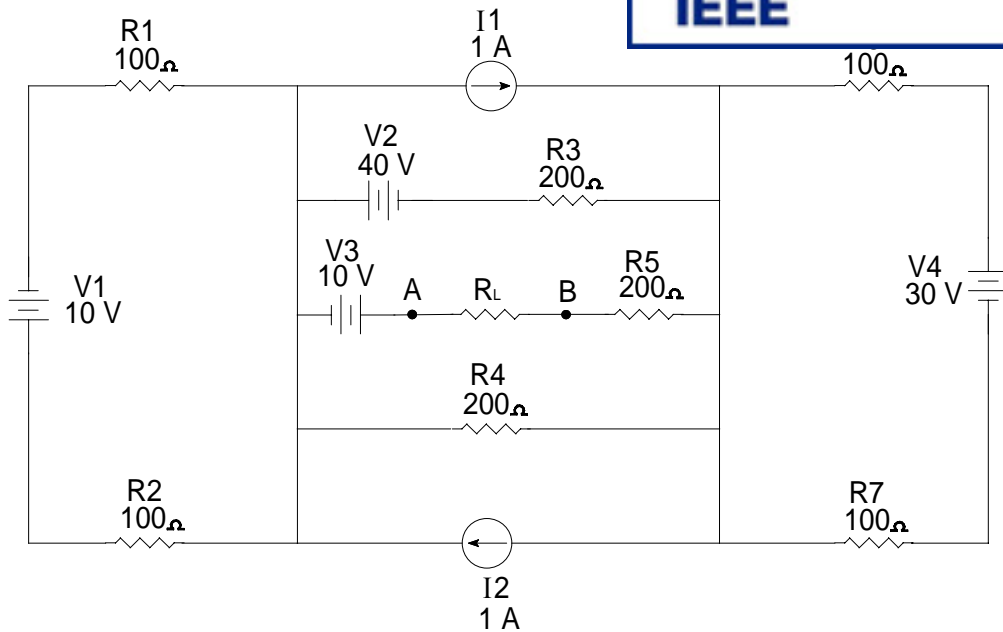


1.

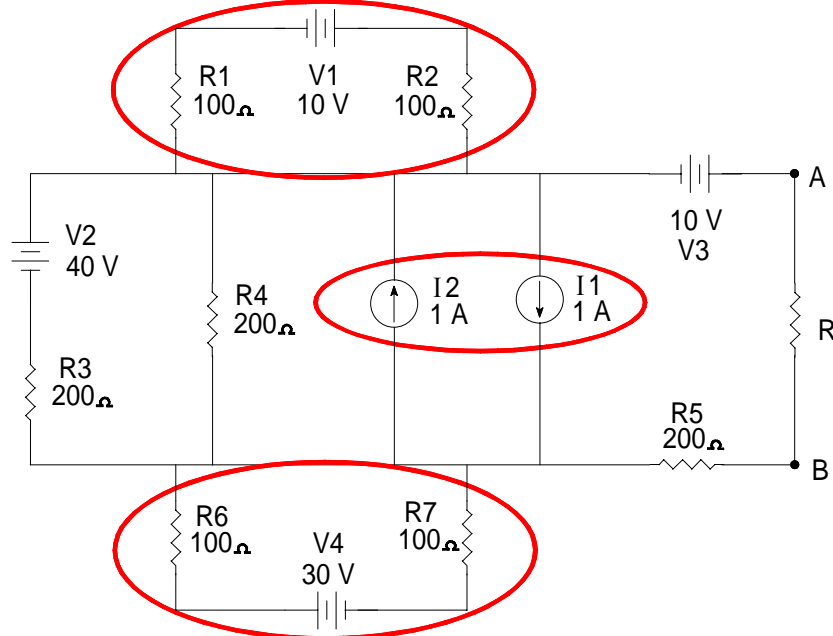


**Figure 1**

a) Determine and sketch the Thevenin's equivalent circuit for the output terminals A and B.

**Solution**

First it would help to redraw the circuit to a more familiar layout.

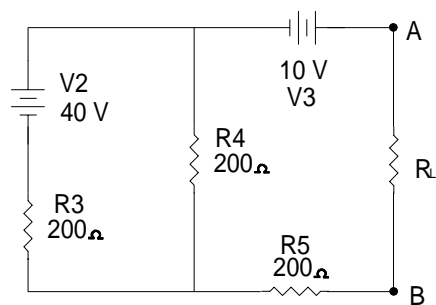


**Figure 1a**

After redrawing the circuit one should see that circuit elements  $V_1$ ,  $R_1$ ,  $R_2$  and  $V_4$ ,  $R_6$ ,  $R_7$  have no effect on the Thevenin's equivalent circuit. As well current sources  $I_1$  and  $I_2$  cancel each other out. Therefore the resulting circuit to determine is shown in Figure 1b

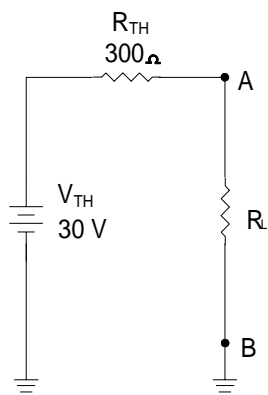
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**Figure 1b**

Obviously the circuit is very simple and the resulting Thevenin's equivalent circuit is...



**Figure 1c** Thevenin's equivalent circuit.

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### Question 1 Continued

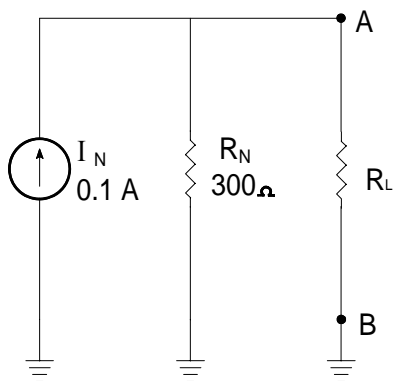
b) What value of load resistance would maximize power transfer?

$$R_L = R_{TH} = 300 \, \Omega$$

c) What is the Norton's equivalent circuit?  
(Provide a circuit sketch as well)

$$R_N = R_{TH} = 300 \, \Omega$$

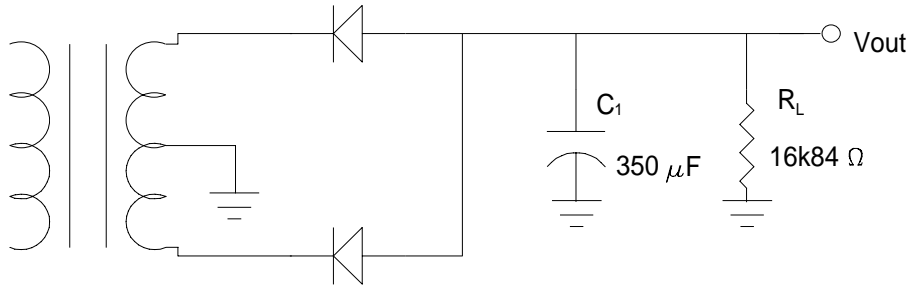
$$I_N = \frac{V_{TH}}{R_{TH}} = 0.1 \text{ A}$$



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2. The output of the power supply shown in Figure 2 has a peak to peak ripple of 300 mV. What is the RMS output of the transformer secondary (total secondary)?



**Figure 2**

Solution:

$$C = \frac{\Delta Q}{\Delta V} = \frac{i_L T}{\Delta V} = \frac{i_L}{\Delta V F} \Rightarrow i_L = C \Delta V F = (350 \mu F)(0.3 V)(120 \text{ Hz}) = 12.6 \text{ mA}$$

$V_L = V_P = (12.6 \text{ mA})(16.84 \text{ k}\Omega) = 212.18 \text{ V}_P = V_P$  for  $\frac{1}{2}$  of the secondary or  $212.88 \text{ V}_P$  if you included the 0.7 Volt drop across the diodes.

Therefore the Full Secondary voltage is  $2 \times 212.18 \text{ V}_P = 425.77 \text{ V}_P$

And the RMS voltage is  $\frac{V_{P \text{ sec}}}{\sqrt{2}} = \frac{425.77 \text{ V}_P}{\sqrt{2}} = 300.07 \text{ V}_{\text{RMS}}$  or  $301.06 \text{ V}_{\text{RMS}}$  if 0.7 V diode drop was taken into account.

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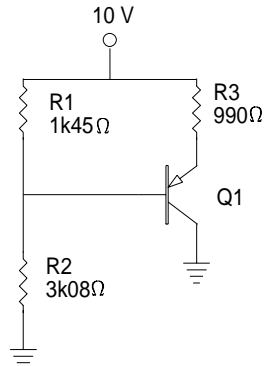
3. a) Why is the arrow on the BJT schematic symbol important?

- Determines the emitter leg.
- Determines the transistor type (NPN or PNP).

b) The condition where an increase in base current will not cause further increases in collector current is called saturation?

c) When a BJT has it's BE junction forward-biased and it's CB junction reversed biased, the transistor is correctly biased.

d) Draw the load line and determine the Q point for the transistor circuit. Assume  $\beta = 100$ ,  $V_{BE} = -0.7 \text{ V}$ , and  $I_{CBO} = 1 \text{ } \mu\text{A}$ .



**Figure 4**

$$I_{C(Sat)} = \frac{V_{CC}}{R3} = \frac{10V}{990\Omega} = 10.1mA$$

$$V_B = V_{CC} \frac{R2}{R1 + R2} = 10V \frac{3.08k\Omega}{3.08k\Omega + 1.45k\Omega} \cong 6.799V$$

$$\therefore V_E = V_B - V_{BE} = 6.799V - (-0.7V) = 7.499V \cong 7.5V$$

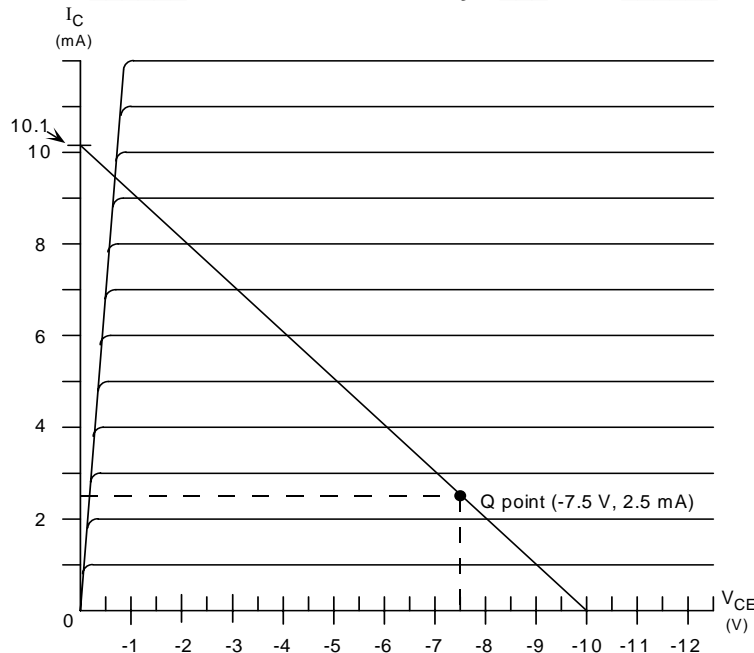
$$V_C = 0V \Rightarrow \therefore V_{CE} = V_C - V_E = 0V - 7.5V = -7.5V = V_{CEQ}$$

$$I_{EQ} = \frac{V_{CC} - V_E}{R3} = \frac{10V - 7.5V}{990\Omega} \cong 2.525mA$$

$$I_{CQ} = \frac{\beta}{\beta + 1} I_{EQ} = \frac{100}{100 + 1} 2.525mA = 2.5mA$$

$$I_{CQ} = \underline{2.5 \text{ mA}}$$

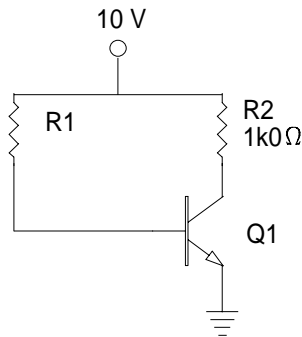
$$V_{CEQ} = \underline{-7.5V}$$



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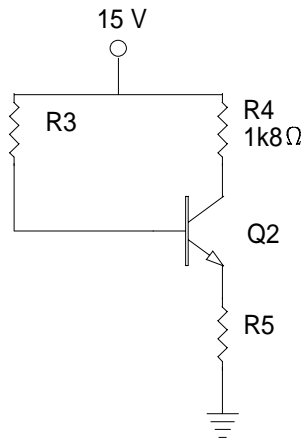
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4. Calculate all resistor values to place the transistors into the middle of their operating region for the circuits shown. Assume  $\beta = 100$ ,  $V_{BE} = 0.7 \text{ V}$ , and  $I_{CBO} = 1 \mu\text{A}$ .



**Figure 5**

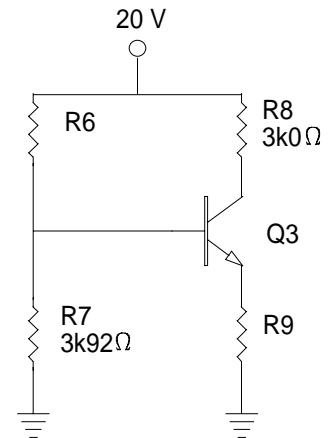
$$R1 = \underline{186k\Omega}$$



**Figure 6**

$$R3 = \underline{452k\Omega}$$

$$R5 = \underline{1k188\Omega}$$



**Figure 7**

$$R6 = \underline{12k76\Omega}$$

$$R9 = \underline{1k98\Omega}$$

First you are designing these so you use the guidelines for quiescent voltages given in class.  $V_{CEQ} = \frac{1}{2} V_{CC}$ , if there are resistors in both the collector and emitter legs then you distribute the voltages as  $0.3V_{CC}$  and  $0.2V_{CC}$  respectively.

For R1

$$I_{CQ} = \frac{V_{CC}/2}{1k0\Omega} = 5mA \Rightarrow \therefore I_{BQ} = \frac{I_{CQ}}{\beta} = 50\mu A$$

$$R1 = \frac{V_{CC} - V_{BE}}{I_{BQ}} = 186k\Omega$$

For R5

$$V_{R4} = 0.3V_{CC} = 4.5V \Rightarrow \therefore I_{CQ} = \frac{4.5V}{1k8\Omega} = 2.5mA \Rightarrow \therefore I_{EQ} = \frac{\beta+1}{\beta} I_{CQ} = 2.525mA$$

$$R5 = \frac{0.2V_{CC}}{I_{EQ}} \cong 1k188\Omega \approx 1k2\Omega$$

For R3

$$I_{BQ} = \frac{I_{CQ}}{\beta} = 25\mu A$$

$$R3 = \frac{V_{CC} - V_{BE} - V_{R5}}{I_{BQ}} = 452k\Omega$$

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For R9

$$V_{R8} = 0.3V_{CC} = 6V \Rightarrow \therefore I_{CQ} = \frac{6V}{3k0\Omega} = 2mA \Rightarrow \therefore I_{EQ} = \frac{\beta+1}{\beta} I_{CQ} = 2.02mA \Rightarrow \therefore V_{R9} = 0.2V_{CC} = 4V$$

$$R9 = \frac{4V}{2.02mA} \cong 1k98\Omega$$

For R6

$$V_{BQ} = V_{R9} + V_{BE} = 4.7V$$

Solving the voltage divider equation for R6 yields;

$$R6 = \frac{20V}{4.7V} 3k92\Omega - 3k92\Omega = 12k76\Omega$$

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### 5. (Use the second approximation of the diode!)

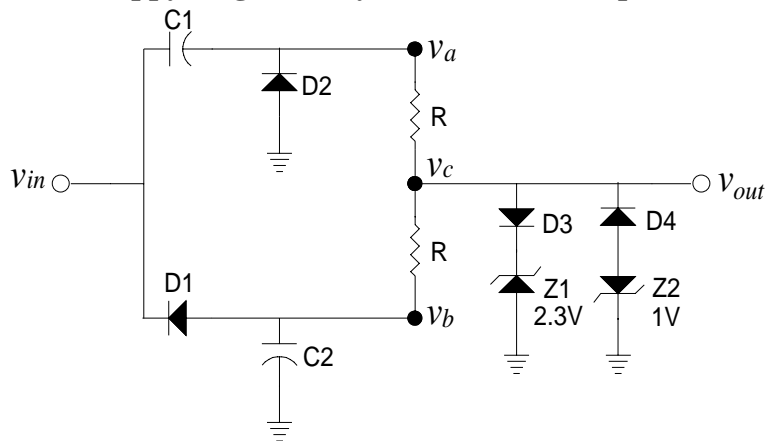
Sketch the waveform at each terminal,  $v_a$ ,  $v_b$ ,  $v_c$ , and  $v_{out}$  on the supplied graphs.

Note:  $v_{in}$  is 10 V<sub>p-p</sub> at 1 kHz and has been supplied on each graph as a reference.

Also determine the waveform at  $v_c$  without diodes D3, D4, Z1, and Z2.

i.e. As an intermediate step to determining the output.

**Please try to be neat! A sloppy diagram may lead to a misinterpretation and lost marks.**



**Figure 3**

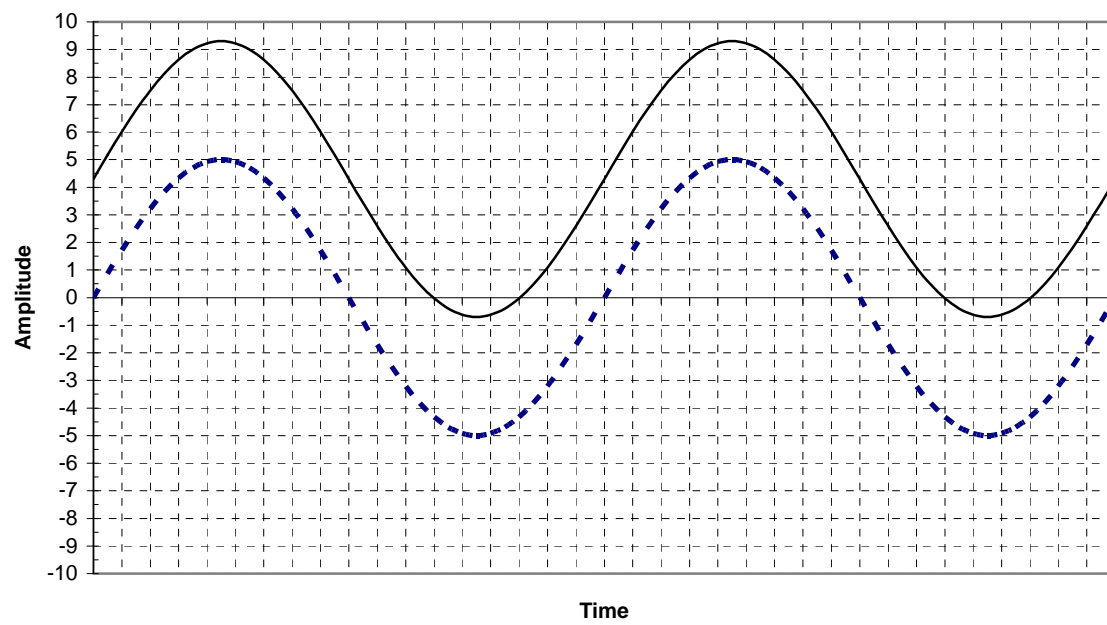
Assume  $\tau$  is Very large.



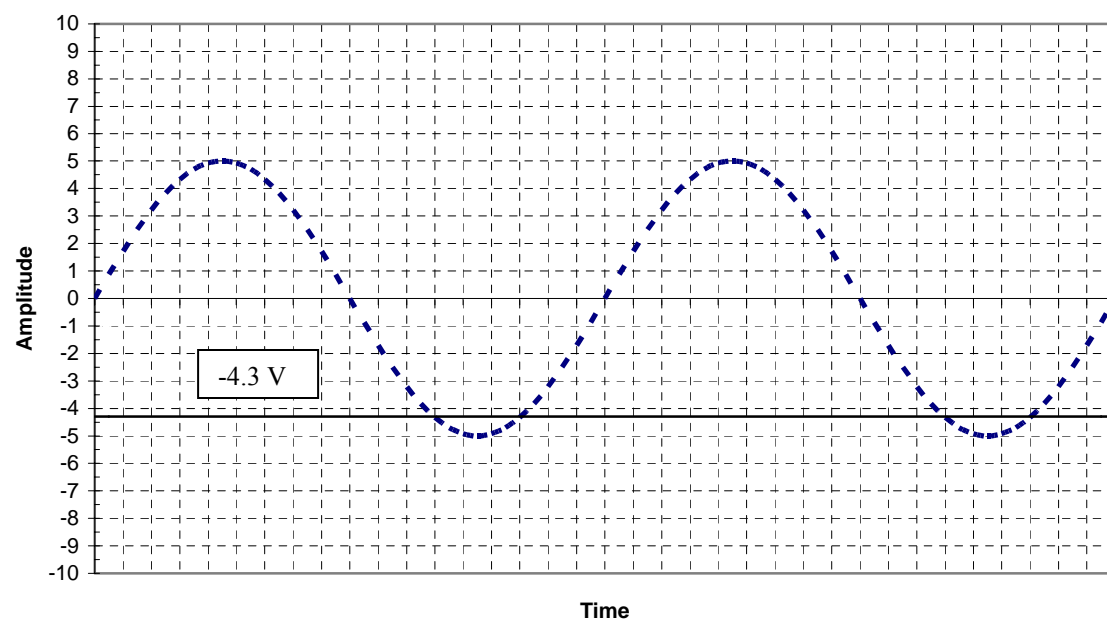
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$v_a$



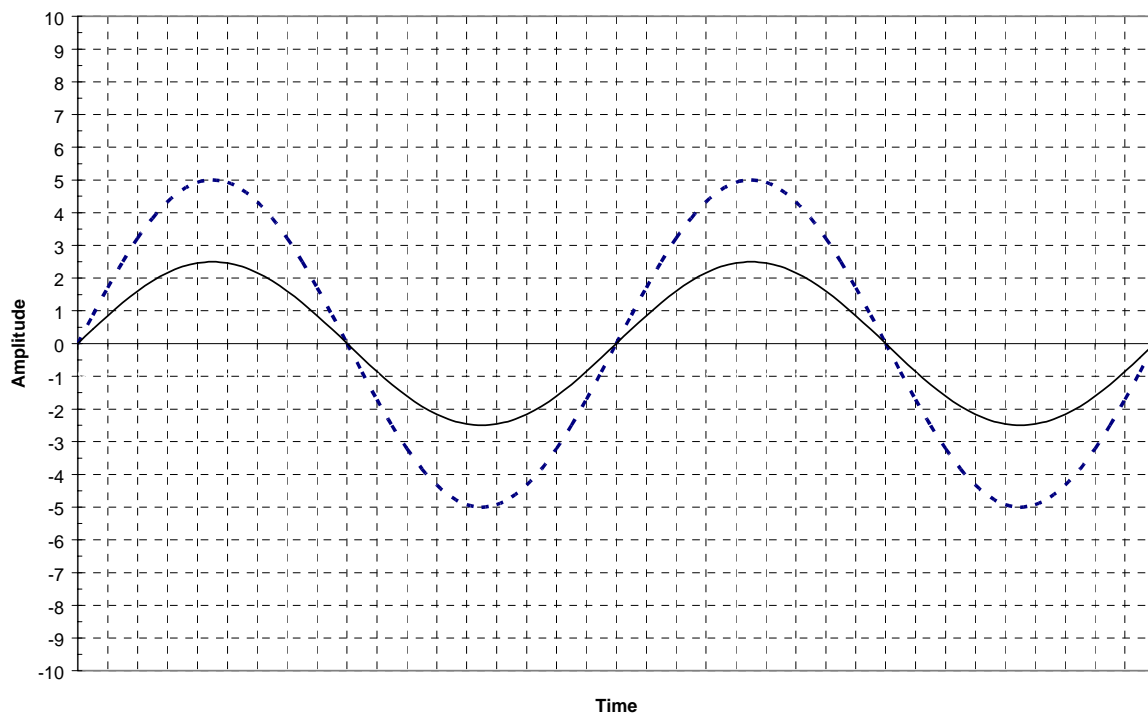
$v_b$



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$v_c$



$v_{out}$

